1	TITLE							
2	Influence of the feed pipe position of an industrial scale two-phase decanter on extraction							
3	efficiency and chemical-sensory characteristics of virgin olive oil							
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5	RUNNING TITLE							
6	Decanter feeding impact on extraction efficiency and olive oil quality							
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25 ABSTRACT 26 BACKGROUND: Nowadays, olive oil extraction is basically made by means of two-phase 27 decanters, which allow to reduce water consumption and leaching of phenolic compounds. 28 Despite this, most of the working settings derive from studies carried out on three-phase 29 decanters. Hence, aim of the present study has been assessing the influence of two-phase decanter feed pipe position (FP) on the extraction efficiency and chemical-sensory 30 31 characteristics of virgin olive oil. Three different positions have been considered, at 825 mm 32 (FP1), 610 mm (FP2), and 520 mm (FP3) from the outlet of the oily phase. 33 RESULTS: Position FP3 allowed the highest oil recovery (up to 10%), the lowest percentage of 34 oil in the olive pomace and, in general, a regular trend in terms of oil extraction efficiency. 35 However, the oily must that came out of the decanter was not completely clean in terms of 36 residual content of solid sediment and water. The feeding position partially affected the profile 37 of antioxidant compounds. 38 CONCLUSION: In two-phase decanters, loading the olive paste close to the outlet of the oily 39 phase is recommended in order to increase the extraction efficiency without jeopardising the 40 chemical-sensory characteristics of virgin olive oil. 41 42 **KEYWORDS** 43 Decanter; Olive oil extraction; Virgin olive oil; Extraction efficiency; Quality.

INTRODUCTION

45 Virgin olive oil production has been deeply studied from the field stage, to the promotion of main product, and including the disposal of the by-products.¹⁻⁵ Over the years, due to the 46 47 discontinuous processing and high management costs, the olive oil extraction system has 48 undergone profound changes: the traditional olive processing by pressure has been replaced by 49 more efficient centrifugation systems based on two-phase and three-phase decanters.^{6,7} 50 However, the latter are known to have disadvantages such as: i) high energy and water 51 consumption for the dilution of olive paste; ii) excessive volume of vegetation water, which 52 causes high disposal costs; iii) loss of minor water-soluble constituents of the oils, in particular phenolic substances; iv) variation of organoleptic characteristics of the oils.^{8,9} 53

54 In addition, Cauteruccio et al. highlighted other critical aspects, due to the thickness of the cloak and to the length and thickness of the auger hollow shaft.¹⁰ The same authors have still found 55 56 difficulties in modelling a machine such as a three-phase decanter, due to its geometry and the 57 composition of the fluid inside it; in fact, the olive paste, depending on the position along the 58 axis, varies considerably its composition in terms of specific weight and density. On the other 59 hand, already in a previous experimental-theoretical study, some parameters such as solid flow 60 coefficient, drag number, and dynamic productivity coefficient have been considered to design the three-phase decanters, further used by Boncinelli et al.^{11,12} This has led to the development 61 62 of the three-phase water-saving decanter, equipped with auger/drum differential speed control systems, and assisted by automatic control mechanisms.¹³ Moreover, the same authors found 63 64 that in order to produce an additional liquid phase separation effect from the solid matrix, the 65 introduction of barriers near the decanter drainage mouth, the use of variable speed screw 66 conveyor, and the modification of the contour cone profile allowed a wide range of processing 67 conditions, such as: water and oil flow rates, differential speed of the cochlea with respect to the drum, drainage levels of the water and oil.¹³ By the proper adjustments of the above parameters, 68 the extraction efficiency was constant in a very wide range of feed rates (1800-2800 kg h⁻¹), 69 higher than the previous decanters, especially at low dilution of the olive paste.¹³ Similar results 70 have been reported recently by Squeo et al.¹⁴ In a study of optimization of a three-phase water-71

saving decanter it was noted that the extraction efficacy was directly related to the time of paste permanence and inversely to the differential speed (ΔN) .¹⁵ Tamborrino et al. investigated, instead, on rheological properties, energy consumption, oil yield, and quality when the calcium carbonate was used during the extraction process.¹⁶

76 The two-phase decanter, on the contrary, has been studied mainly by a qualitative point of 77 view.^{17,18} In particular, Klen et al. evaluated the content of phenols by comparing different 78 extraction systems; Caponio et al. evaluated the chemical composition of extra virgin olive oil 79 in function of the decanter set-up (two- and three-phase) and the differential speeds between drum and cochlea (Δ N16 and Δ N11).^{19,20} Moreover, Giovacchino and co-authors found that by 80 81 using a decanter capable of working at two- and three-phase, comparable yields were obtained 82 when in the two-phase process the feed rate was reduced to 60-70% of the theoretical value 83 advised; Avr et al., instead, highlighted the importance of paste preparation in two-phase separation by studying a fluid-dynamic simulation model adaptable to two-phase extraction.²¹⁻²³ 84 Finally, a study carried out by Tamborrino et al. using an innovative decanter, able to switch 85 86 from three- to two-phase processing without interrupting the extraction, allowed a correlation 87 between the flow rate, the oil outlet level, the drum/cochlea ΔN , and the extraction efficiency.⁷

88 In this framework, the need of a further investigation on the working parameters of the two-89 phase decanter is highlighted, since many of the technical solutions adopted are currently based 90 on those used in three-phase machines. The purpose of this work was therefore to investigate the influence of the position of the olive paste feed pipe (FP) in a two-phase industrial-scale 91 92 decanter capable of working at high feed rates, by evaluating the results in terms of extraction 93 efficiency and chemical-sensory characteristics of the virgin olive oil obtained. Then, three 94 different positions have been considered, at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) 95 from the outlet of the oily phase.

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EXPERIMENTAL

98 Industrial olive oil extraction plant

99 The experimental tests were carried out in an industrial olive oil mill (Cooperativa Produttori 100 Olivicoli) located in Bitonto (Apulia, Italy) using a two-phase decanter (REX250 model, 101 Amenduni Nicola S.p.a., Modugno, Italy). In this decanter, olive paste is fed from the opposite 102 side to the conical section (i.e. the "beach" zone), with the possibility to move the feed pipe 103 through the drum section, depending on the ripeness degree of olives and the need to set the 104 two- (oil and pomace) or three-phase (oil, water, and pomace) mode, which is made possible by 105 the simple adjustment of water and oil levels. The internal screw conveyor rotates faster than the 106 decanter drum, and the residence time of the pomace can be adjusted by varying the differential 107 speed (ΔN).

108 Olive fruits (*Olea europaea* L.) of Coratina cultivar, mechanically harvested in the fifteen last 109 days of November 2016, after leaf-removal, were milled unwashed within 24 h. Two lots of 110 olives were processed in different days, characterized by a maturity index, determined as 111 reported in Squeo et al. equal to 1.07 and 1.39, respectively.²⁴

112 A lot of about 12,000 kg of olives was considered for each trial. Figure 1 shows the flux 113 diagram of olive oil processing. In particular, each olive lot was milled with a hammer-crusher 114 (A60 model, Amenduni Nicola S.p.a., Modugno, Italy) operating at 1,500 rpm, with a 115 processing capacity of 7,000 kg h⁻¹ and grid with holes of 6 mm of diameter, then the olive paste 116 was transferred in the malaxer (6V1000 model, Amenduni Nicola S.p.a., Modugno, Italy). After 117 malaxation (90 min at 27 ± 1 °C), the paste was pumped into a two-phase decanter (REX250 118 model, Amenduni Nicola S.p.A., Modugno, Italy) – operating at 2,800 rpm (bowl) and 2,825 rpm (screw), with a processing capacity of 6,000 kg h⁻¹ without dilution with water – in three 119 120 different feed pipe (FP) positions: at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) from the 121 outlet of the oily phase, as shown in Figure 2. Finally, the oily must was cleaned with a vertical 122 centrifuge (A3500 model, Amenduni Nicola S.p.a., Modugno, Italy), operating at 6,400 rpm and 123 2,000 L h⁻¹. During olive processing, three different samples (every 5 minutes) of oily must 124 (OM), olive pomace (OP), and cleaned oil (O) were collected for each feed pipe position. 125 Moreover, three samples of olive pastes, for each trial, were collected at the end of malaxation 126 step for the viscosity measurements.

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128 Analytical determinations

The viscosity measurements were carried out by a Viscotester VT 550 HAAKE (Thermo Fisher Scientific Inc., Waltham, MA, USA) using 600 mL of olive paste, put into 1,000 mL glass containers and conditioned at same malaxation temperature in a thermostatic bath (27 °C). To interpret the experimental results in terms of viscosity, the acquired torque-speed data and scale readings were converted into shear stress-shear rate relationships using numerical conversion values using the instrument calibration map. The power-law model was used to calculate the apparent viscosity and flow behaviour index from the shear rate using the following Eq (1):

136
$$\eta_{app} = k \gamma^{n-1} \tag{1}$$

137 where η_{app} is the apparent viscosity, γ is the shear rate (s⁻¹), *n* is the flow behaviour index 138 (dimensionless), k is the consistency index (Pa sⁿ). This model is widely used in fluid dynamics 139 analysis when studying biological fluids as the olive paste that is a mixture of three components: 140 olive oil, vegetation water, solid particles. While olive oil and pure water (not vegetation water) 141 are typical Newtonian fluid characterized by a constant viscosity coefficient, olive paste has 142 more complex rheological behaviour. Its viscosity cannot be considered as constant and depends on several parameters.²⁵ The simplest model that can be used for this fluid is just the power-law 143 144 model.

145 The extraction efficiency (EE) was calculated as the ratio between the weight of virgin olive oil 146 (W_{oil}) obtained at the end of the process, and the weight of oil contained in the corresponding 147 olives determined by Soxhlet extraction (W_{olive}) . Results of Eq. (2) were expressed as 148 percentage (%).

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$$EE = \frac{W_{oil}}{W_{olive}} \times 100 \tag{2}$$

The moisture (g 100 g⁻¹) and total oil (g 100 g⁻¹) content of olives and olive pomaces, as well as the free fatty acids (FFA), peroxide value (PV), and spectrophotometric constants of the extracted oil were determined as described in a previous paper.²⁶ The moisture content of oils was determined at 103 ± 2 °C, according to the ISO method 662/2016, while the solid impurity

154 content of the oils was determined after centrifugation at $4,625 \times g$ (SL 16R Centrifuge, Thermo 155 Fisher Scientific Inc., Waltham, MA, USA), and the results were expressed as a percentage ratio.²⁷ The determination of total phenolic compounds by UV spectrophotometry, chlorophylls, 156 157 carotenoids, and tocopherols was carried out as reported in a previous paper.¹⁶ The 158 determination of the phenolic compounds by HPLC was carried out as described in Caponio et 159 al.²⁸ For the determination of the volatile compounds, the oil samples $(1 \pm 0.005 \text{ g})$ were 160 weighed into 20 mL vials, sealed with a screw top aluminium cap and pierceable butyl rubber 161 septa, and submitted to the (SPME/GC-MS) in the conditions reported by Caponio et al.²⁰ The 162 sensory analysis was performed by a trained panel made of eight judges, experienced in olive oil sensory evaluation in accordance with the Commission Regulation (ECC) No 2568/91.29 163

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165 Statistical analysis

166 Results were expressed as mean \pm standard deviation (SD) of three measurements for the 167 analytical determination. Analysis of variance (ANOVA), followed by Tukey HSD test for 168 multiple comparisons was carried out on the experimental data by means of XLStat software 169 (Addinsoft SARL, New York, NY, USA). Differences were considered significant at $p \le 0.05$.

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RESULTS AND DISCUSSION

172 Decanter performance in relation to feed pipe position

173 Figure 3 reports the rheological profiles of the shear stress versus shear rate for each olive paste 174 after 90 min of malaxation. As shown, the apparent viscosity of the samples decreased with the 175 share rate, in accordance to Tamborrino et al., due to the behaviour as pseudoplastic material of the olive paste.¹⁶ The slightly lower values of apparent viscosity of the samples from the second 176 177 trial could be imputable to higher maturity index of the olives, which causes a higher amount of oil in the olives (data not shown) and an easier breaking of tissues and cells.³⁰ This allows an 178 179 increase of the availability of the liquid fraction and, consequently, the separation between the 180 solid and liquid phases within the olive paste and the coalescence of the oil drops.

181 Table 1 reports for each trial the moisture and oil content of the olive pomace after 182 centrifugation with two-phase decanter, as well as the extraction efficiency. The moisture 183 content of the pomace did not vary significantly in relation to the different feeding position of 184 the olive paste in the decanter, while the residual oil content was significantly lower in FP3 185 compared to the other two positions. Extraction efficiency was also significantly higher in FP3, 186 reaching the values of 83.24% in the first trial and 84.32% in the second, confirming the better 187 performances of the FP3 position. Considering the results in both the trials, it is highlighted an 188 average increase of extraction efficiency over FP1 and FP2 above 3%. Such a percentage is 189 relevant in the industrial production of virgin olive oil.

Figure 4 reports the moisture and solid content of the oily must withdrawn at the decanter outlet in the second trial. The oily must obtained with the FP3 position had significantly higher moisture content and impurities than the other two samples (FP1 and FP2), which did not show significant differences between them. In particular, more than 5% of moisture and more than 17% solids were observed in FP3 samples, whereas less than 2% moisture and approximately 8% solids were ascertained in FP1 and FP2 samples.

196 The explanation of such trend could be found in the different resident time experienced by the 197 oily phase in the decanter. In fact, when olive paste is fed in FP3, i.e. the closest position to the 198 oily must outlet, the oily phase has a resident time no long enough to clarify, differently from 199 what happens when the olive paste is fed in a deeper section through the drum, which forces the 200 oily phase to a longer pathway before leaving the decanter (FP1 and FP2). Nonetheless, it is 201 worth to note that no significant difference in content of moisture and impurities was further 202 detected after the oil finishing by means of the vertical centrifuge (data not shown), that is an 203 usual step in the industrial production of virgin olive oil by means of decanters.

In the light of the aforementioned results it is possible to conclude that in two-phase decanter is recommended to load the olive paste close to the outlet of the oily phase. Moreover, it should be considered that in the two-phase decanter, in which the feeding is carried out on the opposite side from the conical end, the feed pipe does not reach such lengths able to reach the best position for the introduction into the decanter (Fig. 2); as a consequence, these machines do not

209 require any vibrational check-ups when working at maximum rotation speed. From a 210 constructive point of view, the vibration of the auger shaft is essentially due to the mass of the 211 reducer to which it is attached and to the auger mass, so it can vibrate depending on the length 212 and thickness. On the other hand, the auger shaft is subjected to several design constraints: the 213 outer diameter can not be increased because it is constrained into the inner diameter of the 214 bearings and, in most cases, increasing the bearing diameter would cause a significant increase 215 of the costs.¹⁰ In the two-phase decanters, in which the feeding occur at the conical side, the 216 possibility of varying the relative rotation speed between the auger and the drum (ΔN) is 217 particularly important, both for flexural equilibrium and for the success of the separation 218 process. Indeed, ΔN is one of the parameters which, acting on the olive paste resident time, can 219 effectively improve the separation efficiency without needing excessive rotational speeds, if 220 appropriately adjusted. In this perspective, for the two-phase process, the position where to feed 221 the olive paste should be preferably on the opposite side of the cone, allowing to move the 222 injection tube into more internal drum sections depending on the physical characteristics of 223 olive paste and according to the possible need to set the machine in the three-phase mode.

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225 Virgin olive oil quality

226 Table 2 shows the results of the chemical and sensory analyses performed on the oils. All 227 samples exhibited acidity, peroxide value and spectrophotometric constant values within the 228 limits set by the rules for the classification of oil as extra virgin, indicating the good quality of 229 the olives used.³¹ In fact, the acidity and peroxide values did not exceed the value of 0.4% and 8 mEq O_2 kg⁻¹, respectively. Slightly higher K_{270} values were observed for the oils of the second 230 231 trial. These latter samples, on the other hand, showed higher average values of lipophilic 232 (carotenoids, tocopherols) and hydrophilic (phenolic compounds) antioxidants, as well as more 233 marked pungent sensory notes, compared to those of first trial.

The feeding position did not cause substantial changes in the chemical profile, as well as in the sensorial characteristics of the oils. Significantly influenced, in fact, were only the lipophilic antioxidant compounds and, in one of the trials, the pungent note and the content of 237 chlorophylls. Differently, the phenolic content of the oils was not significantly influenced by 238 machine setting. In any case, although without statistical significance, in both the trials FP3 239 samples approximately showed a 10% lower phenolic content than FP1 and FP2. This result 240 could be explained by considering the composition of the oily must. In fact, as shown in Figure 241 4, the oily must obtained from FP3 position had a significantly higher content of water and 242 solids. Given the great affinity of the phenolic compounds for the aqueous phase it can be 243 thought that they are preferably distributed in the latter and therefore lost with it in the 244 subsequent processing step of oil finishing by vertical centrifuges.

245 Carotenoids are a group of tetraterpenoids consisting of isoprene units, and are important liposoluble antioxidants present in oils and fats.³² FP1 feeding caused a significant reduction in 246 247 carotenoids content respect to both FP2 and FP3 in the second trial, and to FP2 in the first trial. 248 This result can be explained considering the low polarity of these compounds and the behaviour 249 of the pomace in the decanter. In fact, FP1 position caused a quick discharge of the pomace 250 from the decanter and therefore made the pomace retain a significantly higher amount of oil 251 compared to other feeding positions (Table 1). Thus, given the carotenoids affinity for the oily 252 phase, it can be supposed that their dissolution in the pomace was higher in the FP1 samples 253 than in the others.

A similar trend was found for α -tocopherol and, consequently, for the total tocopherols, representing the former about 90% of total tocopherols in virgin olive oils.³³ In particular, the FP2 oil had significantly higher content of tocopherols than FP1, in both the trials. This may be due to the chemical characteristics of these compounds which, similarly to carotenoids, have hydrophobic character. However, unexpectedly, a decrease in the tocopherols content was also observed in the FP3 oils compared to the FP2 samples.

Regarding the sensory characteristics of the oils, there was a significant influence of the decanter feed pipe position on the pungent note in the case of the first trial, with significantly higher values for the FP2 samples, according to the highest total phenolic content observed in the same samples. The chlorophyll content showed a significant difference only in the second trail for FP1 samples, which had a higher content than the others.

265 Table 3 shows the content of the individual phenolic compounds determined by HPLC. The oils 266 from the second trial had a higher average content of phenolic compounds compared to the first 267 trial. Overall, the feed pipe position of the olive paste in the decanter has weakly affected the 268 phenolic profile. Consistently with total phenols (Table 2), FP3 position caused a reduction of 269 the phenolic content, significant in the first trial. This result was a consequence of the 270 significant decrease in some of the derivative forms of secoiridoids, in particular the dialdehydic 271 form of the elenolic acid linked to the hydroxytyrosol (3,4-DHPEA-EDA) and tyrosol (p-272 HPEA-EDA), known to be among the most abundant in virgin olive oils.³⁴ In particular, the 273 dialdehydic form of elenolic acid linked to the tyrosol (p-HPEA-EDA), also known as 274 oleocanthal, has long been recognized as the main responsible for the pungency of virgin olive 275 oils and associated with anti-inflammatory activity similar to that of ibuprofen.³⁵ Nevertheless, 276 in our study no straight correlation has been observed between oleocanthal and samples pungent 277 note (Table 2). In the case of the second trail, the only significant differences involved vanillic 278 acid and apigenin. However, a trend similar to that found for the first trial was observed for 3,4-279 DHPEA-EDA, but not for the oleocanthal.

Table 4 shows the volatile compounds found in oils. In both the trails, *trans*-2-hexenal was the most abundant compound, as widely documented in literature.^{28,36,37} The feed pipe position did not lead to significant changes in the volatile profile and only a few significant differences were observed. Also for volatiles, the behaviour was different in the tests suggesting a possible influence of the ripening degree of olives.

285 Considering the first trial, loading the olives paste in FP1 resulted in a significant decrease in 286 trans, trans-2,4-hexadienal, 1-penten-3-one and a significant increase in 1-hexanol, the latter 287 only with respect to FP2 test. Further, the FP2 test showed significantly higher values of ethyl 288 acetate, probably linked to the particular batch of olives used, although derived from a 289 homogeneous batch, and 1-penten-3-one. The FP3 test had significantly lower values of 2-290 methyl-4-pentenal, 1-penten-3-one and limonene respect to the others. In the second trial, 291 significant decreases of ethanol, trans-2-hexen-1-ol and ethyl acetate were observed in FP1, 292 while only trans-3-hexen-1-ol acetate in FP2. Finally, FP3 oils had significantly higher content of ethanol and *trans*-3-hexen-1-ol acetate. Tentatively, the explanation of what observed might
be linked to the polarity of the volatile compounds, similarly to what observed for phenolics.
Indeed, more polar groups such as esters and aldehydes could be more likely found in FP3 oils,
richer in water at exit from the decanter, than the other samples. However, such behaviour was
not observed in both the trials and it was more evident and statistically significant only in the
case of trial II.

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CONCLUSIONS

301 Considering the results about the performances of the two-phase decanter, with the olives used 302 in this experimental study, the position of the feed pipe tube closer to the oil discharge section 303 (FP3) allowed to reach the highest oil recovery and a regular trend in terms of extraction 304 efficiency. On the other hand, the extracted oil was found to contain more sediment and water. 305 The farthest positions from the liquid exit are the worst considering the extraction efficiency, 306 but make it possible to have cleaner oil, although the cleaning of the oily must, carried out in the 307 vertical separator, is usually included in any olive processing plant.

308 Interestingly, our findings highlighted as the different decanter feeding position is also able to 309 influence the balance of lipophilic/hydrophilic antioxidants in the oils. In fact, when the olive 310 paste feeding takes place nearest to the solid discharge (FP1), the resulting oil is richer in 311 phenols and contains less tocopherols and carotenoids than the opposite FP3 position.

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CONFLICT OF INTERESTS

The authors declare that there is no conflict of interests regarding the publication of this paper. Lucio Brunetti, Pasquale Catalano, and Biagio Bianchi edited the "Decanter performance in relation to feed pipe position" section; while Francesco Caponio, Giacomo Squeo, Antonella Pasqualone, Carmine Summo, and Vito M. Paradiso edited the "Virgin olive oil quality" section.

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ACKNOWLEDGEMENTS

321 The authors would like to acknowledge the support of AMENDUNI S.r.l. who provided insight

322 and expertise that greatly assisted the research with their technical staff. We are also grateful to

323 Cooperativa Produttori Olivicoli olive oil mill sited in Bitonto (Bari, Apulia) for supplying the

324 experimental tests.

- 325 This work has been supported by AGER 2 Project, grant n° 2016-0105
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- 327 FIGURE CAPTION
- **328** Figure 1. Experimental plan and sampling points.
- **Figure 2.** Different positions of the decanter feed pipe, at 825 mm, 610 mm, and 520 mm from
- the outlet of the oily phase.
- **331** Figure 3. Shear stress versus shear rate of three olive pastes (P1, P2, P3) collected in two

different olive processing trials. First trial (I-T) corresponded to olives having maturity indexlower than those of second trial (II-T).

334 Figure 4. Moisture and insoluble impurity content of the oily must obtained in an olive

processing trial with olives having a maturity index of 1.39 (second trial) (*n*=3). Three different

- decanter feed pipe (FP) positions were considered, positioned at 825 mm (FP1), 610 mm (FP2),
- and 520 mm (FP3) from the outlet of the oily phase.

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Table 1. Pomace moisture, pomace oil content and oil extraction efficiency (n=3) determined in two different olive processing trials. First trial corresponded to olives having maturity index lower than those of second trial. Three different decanter feed pipe (FP) positions were considered, at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) from the outlet of the oily phase.

Trial	Pomace moisture (%)	Pomace oil content (% d.m.)	Oil extraction efficiency (%)		
I trial					
FP1	62.11±0.89 a	8.89±0.25 a	75.32±0.40 c		
FP2	62.78±0.65 a	8.58±0.10 ab	77.71±0.21 b		
FP3	62.14±1.55 a	8.17±0.32 b	83.24±1.36 a		
II trial					
FP1	63.42±1.16 a	8.42±0.47 a	81.60±1.26 b		
FP2	65.02±3.03 a	8.62±0.57 a	82.71±1.48 ab		
FP3	63.56±1.35 a	7.60±0.12 b	84.32±0.55 a		

Different letters on the same row for the same trial indicate significant differences ($p \le 0.05$) according to one way ANOVA followed by Tukey's HSD test.

Table 2. Mean values, standard deviations and results of the one way ANOVA followed by Tukey's HSD test of the chemical and sensory analyses performed on the oils (n=3) obtained in two different olive processing trials. First trial (I) corresponded to olives having maturity index lower than those of second trial (II). Three different decanter feed pipe (FP) positions were considered, at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) from the outlet of the oily phase.

Trial	Ι			II		
Sample	FP1	FP2	FP3	FP1	FP2	FP3
FFA (g 100g ⁻¹ oleic acid)	0.37±0.00 a	0.37±0.00 a	0.37±0.00 a	0.37±0.00 a	0.37±0.00 a	0.37±0.00 a
$PV (mEq O_2 kg^{-1})$	8.0±0.8 a	7.7±1.0 a	7.8±0.5 a	6.7±0.9 a	6.4±0.7 a	6.6±1.1 a
K ₂₃₂	1.70±0.02 a	1.71±0.04 a	1.69±0.04 a	1.67±0.03 a	1.66±0.03 a	1.73±0.12 a
K ₂₇₀	0.17±0.03 a	0.17±0.05 a	0.18±0.04 a	0.19±0.02 a	0.20±0.03 a	0.22±0.08 a
TPC (mg kg ⁻¹)	356±28 a	387±41 a	314±26 a	480±23 a	460±27 a	433±7 a
Chlorophylls (mg kg ⁻¹)	15.72±0.81 a	16.04±0.03 a	16.41±0.14 a	15.56±1.45 a	13.30±0.24 ab	13.09±0.76 b
Carotenoids (mg kg ⁻¹)	12.34±1.33 b	14.22±1.68 ab	16.50±0.57 a	12.88±2.32 b	18.54±2.43 a	18.03±0.88 a
β + γ -Tocoferols (mg kg ⁻¹)	3.71±0.40 a	4.41±0.39 a	4.37±0.15 a	5.28±0.03 a	5.75±0.23 a	5.24±0.51 a
α-Tocoferol (mg kg ⁻¹)	159.37±1.37 b	163.93±1.58 a	162.07±1.79 ab	170.16±0.99 ab	172.27±0.07 a	169.25±1.14 b
Tocoferols (mg kg ⁻¹)	163.08±1.75 b	168.35±1.95 a	166.44±1.91 ab	175.44±0.96 b	178.02±0.23 a	174.49±1.15 b
Fruity*	3.5±0.7 a	5.0±0.7 a	4.3±0.5 a	3.6±0.5 a	3.8±0.6 a	3.5±0.7 a
Bitter*	2.2±0.3 a	2.6±0.7 a	1.7±0.5 a	2.5±0.2 a	2.5±0.4 a	2.1±0.2 a
Pungent*	2.3±0.1 a	3.2±0.6 a	2.2±0.6 a	3.3±0.3 a	2.4±0.1 a	2.8±0.4 a

FFA, free fatty acids; PV, peroxide value; K_{232} , specific absorption at 232 nm; K_{270} , specific absorption at 270 nm; TPC, total phenolic content. *Median ± robust standard deviation (Regulation ECC No 2568/91). Statistical significance was determined by Kruskal-Wallis test ($p \le 0.05$). Different letters on the same row for the same trial indicate significant differences ($p \le 0.05$).

Table 3. HPLC phenolic profile (mg kg⁻¹ \pm sd) of the oils obtained in two different olive processing trials (*n*=3). First trial (I) corresponded to olives having maturity index lower than those of second trial (II). Three different decanter feed pipe (FP) positions were considered, at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) from the outlet of the oily phase.

Trial	Ι			П		
Sample	FP1	FP2	FP3	FP1	FP2	FP3
Hydroxytyrosol	0.28±0.02 a	0.28±0.03 a	0.25±0.05 a	0.54±0.10 a	0.58±0.10 a	0.56±0.04 a
Tyrosol	0.47±0.02 a	0.46±0.04 a	0.47±0.01 a	0.66±0.09 a	0.75±0.05 a	0.76±0.02 a
Vanillic acid	0.20±0.06 a	0.19±0.04 a	0.22±0.05 a	0.22±0.01 ab	0.20±0.02 b	0.25±0.01 a
Syringic acid	0.35±0.04 a	0.37±0.05 a	0.37±0.03 a	0.32±0.07 a	0.32±0.09 a	0.33±0.08 a
3,4-DHPEA-EDA	28.26±0.68 a	28.13±1.33 a	21.86±0.74 b	28.47±4.47 a	24.89±4.71 a	23.27±1.31 a
Oleuropein	1.43±0.27 a	1.34±0.20 a	1.03±0.05 a	2.73±0.29 a	2.52±0.87 a	2.18±0.15 a
<i>p</i> -HPEA-EDA	25.35±0.26 ab	25.70±0.85 a	23.89±0.70 b	25.49±1.15 a	26.51±0.27 a	26.31±0.48 a
(+)-Pinoresinol	10.36±0.23 a	10.90±0.22 a	10.05±0.54 a	12.26±0.54 a	12.44±0.15 a	12.09±0.20 a
1-Acetoxypinoresinol	0.86±0.03 a	1.02±0.05 a	1.00±0.22 a	2.38±0.16 a	2.61±0.19 a	2.28±0.11 a
Cinnamic acid	0.43±0.24 b	0.91±0.10 a	1.14±0.21 a	1.94±0.43 a	2.32±0.36 a	2.42±0.13 a
3,4-DHPEA-EA	4.75±0.25 a	4.78±0.10 a	4.43±0.20 a	4.43±0.41 a	4.98±0.16 a	4.60±0.16 a
Luteolin	3.65±0.46 a	3.95±0.43 a	3.24±0.26 a	4.14±0.37 a	4.38±0.60 a	4.50±0.36 a
<i>p</i> -HPEA-EA	3.54±0.17 a	3.70±0.26 a	3.65±0.18 a	3.30±0.06 a	3.55±0.31 a	3.31±0.17 a
Apigenin	6.07±0.06 a	6.41±0.35 a	6.02±0.17 a	4.13±0.05 b	4.36±0.03 a	4.19±0.05 b
Total	86.00±0.18 a	88.15±3.49 a	77.61±2.10 b	91.01±7.89 a	90.39±6.14 a	87.05±2.43 a

3,4-DHPEA-EDA, dialdehydic form of elenolic acid linked to hydroxytyrosol; *p*-HPEA-EDA, dialdehydic form of elenolic acid linked to tyrosol; 3,4-DHPEA-EA, oleuropein aglycon; *p*-HPEA-EA, ligstroside aglycon.

Different letters on the same row for the same trial indicate significant differences ($p \le 0.05$) according to one way ANOVA followed by Tukey's HSD test.

Table 4. Profile of volatile compounds (mg kg⁻¹ \pm sd) of the oils obtained in two different olive processing trials (*n*=3). First trial (I) corresponded to olives having maturity index lower than those of second trial (II). Three different decanter feed pipe (FP) positions were considered, at 825 mm (FP1), 610 mm (FP2), and 520 mm (FP3) from the outlet of the oily phase.

	Trial	Ι			II		
	Sample	FP1	FP2	FP3	FP1	FP2	FP3
Aldehydes	Hexanal	8.34±0.93 a	7.88±0.91 a	7.67±0.64 a	7.57±1.48 a	8.10±0.99 a	10.21±0.48 a
	cis-3-Hexenal	5.30±0.55 a	4.81±0.81 a	5.07±1.24 a	4.78±1.50 a	6.58±0.68 a	5.41±0.16 a
	trans-2-Hexenal	232.90±25.53 a	222.80±32.64 a	225.15±21.93 a	177.08±25.01 a	195.70±17.34 a	217.63±5.37 a
	3-Metilbutanal	0.28±0.06 a	0.35±0.05 a	0.24±0.03 a	0.03±0.03 b	0.12±0.01 a	0.09±0.00 a
	trans-2-Pentenal	1.33±0.13 a	1.17±0.18 a	1.20±0.29 a	1.20±0.29 a	1.38±0.16 a	1.63±0.20 a
	Nonanal	0.84±0.12 a	0.94±0.15 a	0.62±0.20 a	0.28±0.10 a	0.25±0.04 a	0.28±0.10 a
	trans, trans-2.4-Hexadienal	2.70±0.46 b	4.92±0.93 a	4.34±0.40 a	3.39±1.47 a	4.82±0.45 a	2.94±0.31 a
	2-Metil-4-pentenal	6.80±0.78 a	6.23±0.81 a	0.65±0.09 b	5.98±1.70 a	6.60±1.05 a	7.07±0.36 a
Alcohols	Ethanol	1.68±0.60 a	1.61±0.24 a	1.01±0.21 a	1.31±0.48 b	1.79±0.47 ab	2.97±0.58 a
	trans-2-Hexen-1-ol	1.66±0.29 a	1.65±0.25 a	2.02±0.32 a	0.84±0.41 b	2.40±0.94 a	3.41±0.16 a
	1-Hexanol	1.85±0.32 a	1.05±0.18 b	1.37±0.16 ab	2.12±0.51 a	1.77±0.71 a	1.65±0.68 a
Esters	trans-3-Hexen-1-ol acetate	4.60±0.50 a	4.98±0.84 a	4.31±1.26 a	4.21±0.37 ab	3.56±0.52 b	5.01±0.68 a
	Ethyl acetate	0.68±0.04 b	1.11±0.16 a	0.67±0.16 b	0.45±0.06 b	0.71±0.03 a	0.72±0.08 a
	cis-3-Hexenil acetate	0.00 ± 0.00	0.00 ± 0.00	0.00 ± 0.00	0.00±0.00 a	0.13±0.23 a	0.00±0.00 a
	Metil acetate	0.06±0.11 a	0.19±0.17 a	0.20±0.06 a	0.18±0.07 a	0.20±0.08 a	0.24±0.01 a
Ketones	1-Penten-3-one	9.99±0.61 b	12.03±0.82 a	7.24±0.56 c	8.88±2.83 a	9.96±1.80 a	12.57±0.99 a
	3-Pentanone	1.34±0.14 a	1.48±0.26 a	1.14±0.22 a	1.01±0.44 a	1.26±0.23 a	1.50±0.17 a
Acids	Acetic acid	1.04±0.57 a	0.73±0.07 a	1.95±1.94 a	0.00±0.00 a	0.00±0.00 a	0.00±0.00 a
Others	Octane	0.82±0.14 a	1.08±0.19 a	1.14±0.53 a	0.56±0.09 a	0.62±0.15 a	0.59±0.07 a
	Limonene	0.53±0.03 a	0.56±0.05 a	0.40±0.06 b	0.56±0.16 a	0.69±0.11 a	0.80±0.13 a
Total		282.75±28.97 a	275.57±38.81 a	266.38±24.49 a	220.43±25.73 b	246.63±21.12 ab	274.72±7.77 a

Different letters on the same row for the same trial indicate significant differences ($p \le 0.05$) according to one way ANOVA followed by Tukey's HSD test.